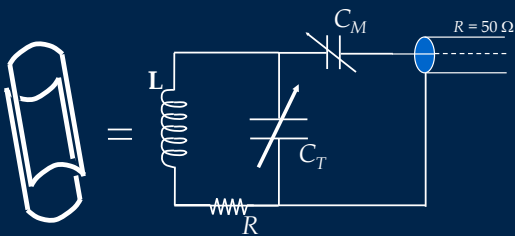


# Introduction to MR Hardware

## RF Coils

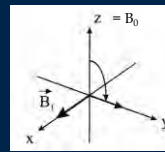
Dominik v. Elverfeldt  
Sep 5<sup>th</sup> 2012



$$\omega = \gamma \cdot B_0$$

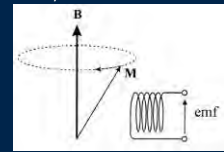
$$\omega = \frac{1}{\sqrt{L \cdot C_T}}$$

### Transmission



- Oscillating with Larmor frequency  $\omega$ .
- $B_1$  - field perpendicular to  $M$
- $\alpha = -\gamma \cdot B_1 \cdot t_{\text{pulse}}$   
e.g.  $90^\circ, 100\mu\text{s} \rightarrow \sim 10^{-4} \text{ T}$
- $\sim \text{W} - \text{kW}$

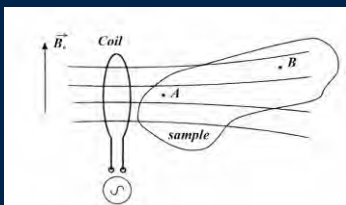
### Reception



- Rotating magnetization produces alternating magnetic field
- Induces electromotive force (emf): principle of induction  
 $U_{\text{ind}} \sim \gamma B_0 \cdot B_{1,xy} \cdot M_0$
- $\sim \mu\text{W} - \text{mW}$

### Reciprocity Theorem

The sensitivity of a magnetic resonance assembly, used as a receiver, to nuclides present at a point A is proportional to that assembly's efficiency, when used as a transmitter, to generate at that same location A a radiofrequency field  $B_1$ .



### RF-coil requirements

- Low distortion of the  $B_0$  field
- Mechanical stability
- Comfortable access to the sample
- Homogeneous  $B_1$  field
- High SNR

## SNR

Signal:

$$U_{ind} \sim \gamma B_0 \cdot B_{1,xy} \cdot M_0$$

Noise:

$$U_{R,eff} = \sqrt{4 \cdot kT \cdot \Delta \nu \cdot R}$$

$$R = R_{coil} + R_{object}$$

$$R_{coil} = R_{johnson} + R_{skin} + R_{prox}$$

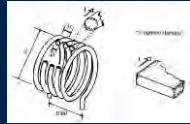
$$R_{object} = R_{mag} + R_{el}$$

$R_{johnson}$

- Brownian motion
- Heat dissipated

$R_{skin}$

- AC flows in a skin on the wires surface
- Decrease of effective wire cross section
- Skin depth:  $\delta \sim \omega_0^{-1/2}$



$R_{prox}$

- Crosstalk between close conductors through emf
- May increase R up to 10 times
- Coil geometry dependent

## SNR

Signal:

$$U_{ind} \sim \gamma B_0 \cdot B_{1,xy} \cdot M_0 \sim B_0^2$$

Noise:

$$U_{R,eff} = \sqrt{4 \cdot kT \cdot \Delta \nu \cdot R}$$

$$R = R_{coil} + R_{object}$$

$$R_{coil} = R_{johnson} + R_{skin} + R_{prox}$$

$$R_{object} = R_{mag} + R_{el}$$

$R_{mag}$

- RF induces currents in conductive material
- Dissipated transmit power
- $R_{mag} \sim b^5$ !
- Noise mechanism during reception
- Dominant effect for high fields and large samples

$R_{el}$

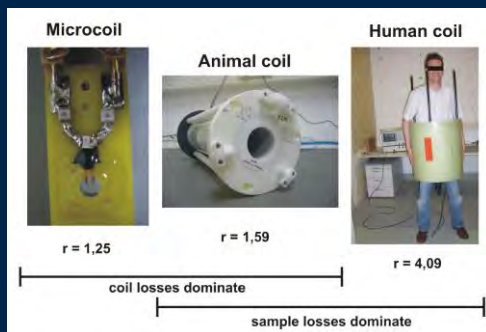
Near field:

- Dissipative displacement currents in dielectric media

Far Field

- Energy loss due to far field radiation
- Only for large coils at very high fields

## $R_{coil}$ vs $R_{object}$



Courtesy of Hans Weber, Freiburg

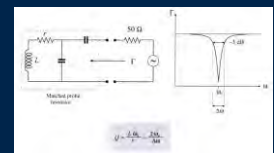
## The quality factor Q

$$Q = 2\pi \cdot \frac{\text{Energy stored in circuit}}{\text{Energy lost per cycle}} = L_{coil} \omega_0 / R = 2\omega_0 / \Delta\omega$$

→ Measure for resistive losses

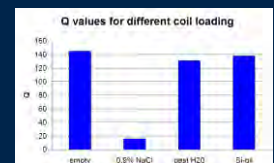
Via Network analyzer:

- $S_{11}$  measurement



Relative contributions of loss mechanisms:

$$Q_{\text{damping ratio}} = Q_{\text{unloaded}} / Q_{\text{loaded}}$$



## Coil Design

The ideal coil structure:

- Sphere with surface currents parallel to equator, sinusoidally modulated:

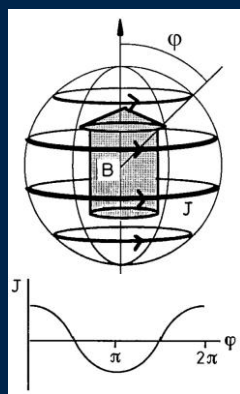
$$J(\phi) \sim \sin \phi$$

Drawbacks:

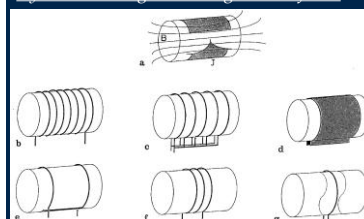
- Spherically limited sample shape
- Limited access to sensitive Volume

Better are cylindrical geometries with

- Longitudinal Fields
- Transversal Fields

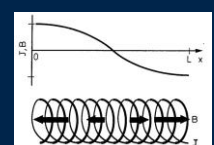


## Cylindrical designs with longitudinal fields

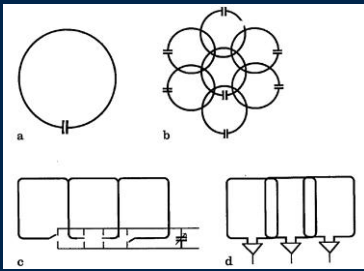


Drawbacks:

- Geometry conflicts created field needs to be perpendicular to  $B_0$  → limited access in biomedical applications
- Self-resonance Standing wave effects, if the total solenoid length approaches the wavelength  $\lambda = 2\pi c / \omega$ .



### Surface array coils

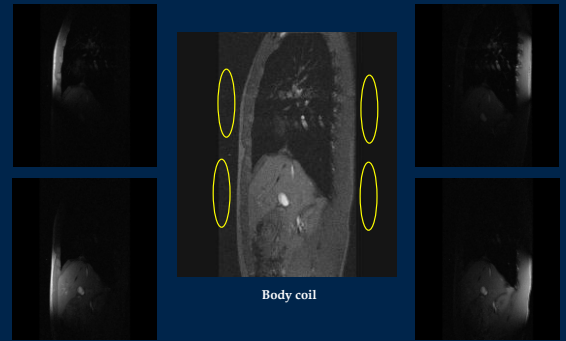


- Single surface coil
- Petal resonator
- Switched-array coil
- Phased-array coil

#### Advantages:

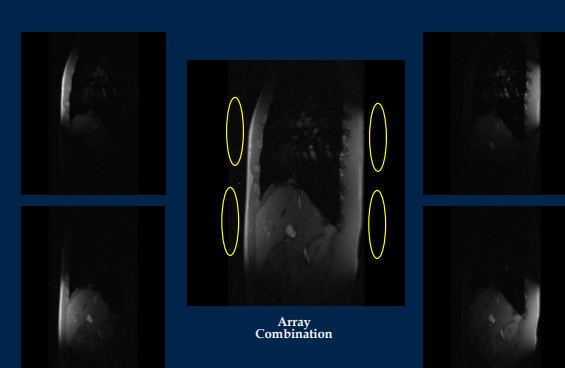
- Planar field of view adaptable to the region of interest
- Increased SNR
- Option for parallel imaging techniques

### Phased array coils



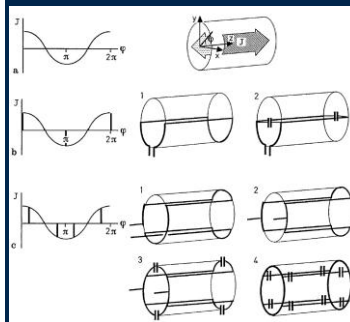
Courtesy of Michael Bock, Heidelberg + Freiburg

### Phased array coils



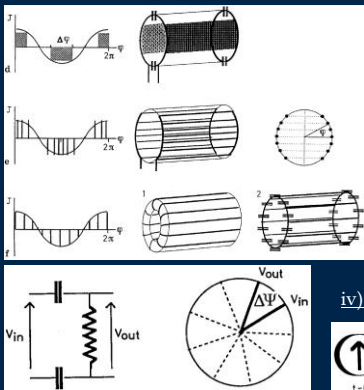
Courtesy of Michael Bock, Heidelberg + Freiburg

### Cylindrical designs with transversal fields I



- Ideal surface current  
 $J = J_0 \cos \varphi z \rightarrow B_1 = (0, B_1, 0)$
- Single loop  
@ highest current density
- Saddle resonator  
Mimics ideal current distribution @ 6 positions.

### Cylindrical designs with transversal fields II



- Alderman-Grant coil
- Filament approx.
- The Birdcage coil (2)

$$i) \Delta \Psi(\omega)$$

$$ii) N * \Delta \Psi(\omega) = 2\pi$$

$$iii) J_n = J_0 \cos(\varphi_n - \omega t)$$

$$iv) B_1 = B_1(\sin \omega t, \cos \omega t, 0)$$

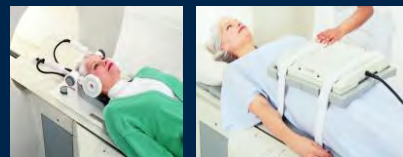


### Human RF - Coils

- Volume Coils



- Surface Coils



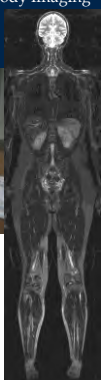
Courtesy of Michael Bock, Heidelberg + Freiburg

## Human RF - Coils

- Phased Array - Head
- Phased Array Body



- Whole Body Imaging

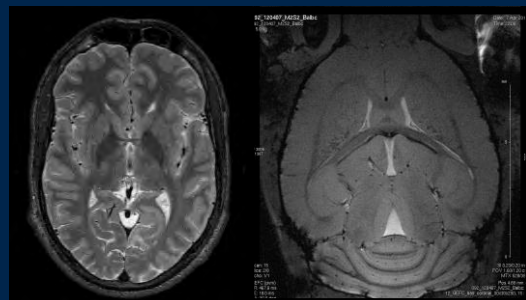


Courtesy of Michael Bock, Heidelberg + Freiburg

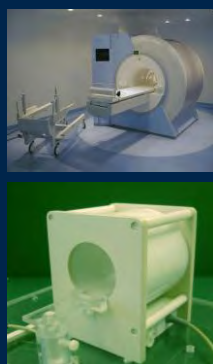
## From Men to Mice

Volume/SNR - Reduction from  $\sim(1\text{mm})^3$  to  $(100\mu\text{m})^3$  equals factor  $>100$

Compensation: Higher B0 Fields, dedicated RF - coils



## Small animal RF - Coils: In human MR-Systems



### Advantages

- Transferability of image contrast
- Usage of standard imaging protocols
- Large magnet bore  
→ Multi animal scanning
- Availability

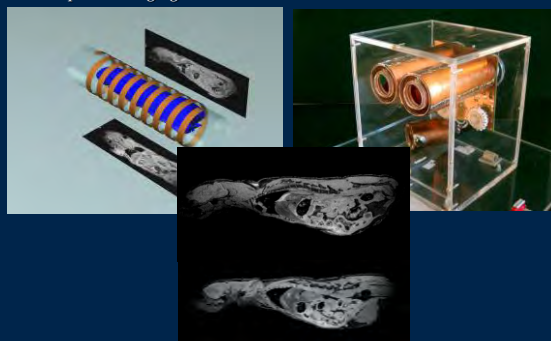
### Drawbacks

- Low SNR → high  $t_{acq}$
- Weak gradients
- Low T2\* contrast
- Hygiene
- High costs

Courtesy of Michael Bock, Heidelberg + Freiburg

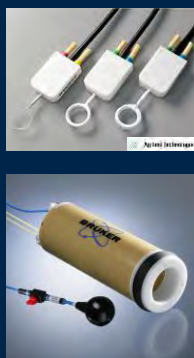
## Small animal RF - Coils: In human MR-Systems

- Isotropic 3D-Imaging



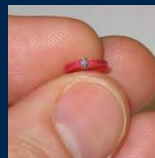
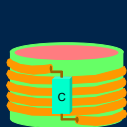
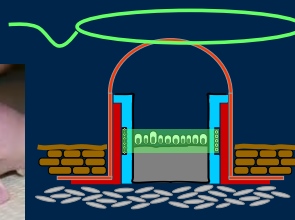
Courtesy of Michael Bock, Heidelberg + Freiburg

## Common small animal RF - Coils



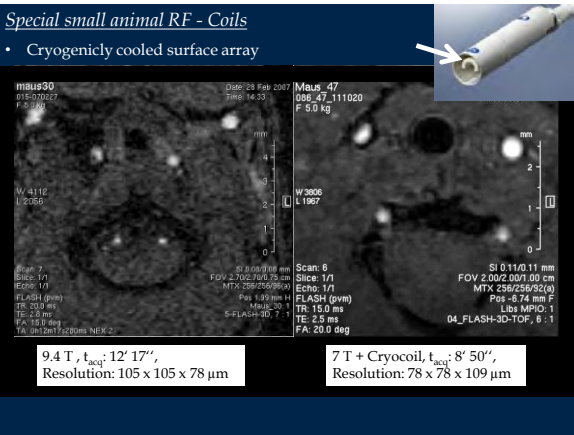
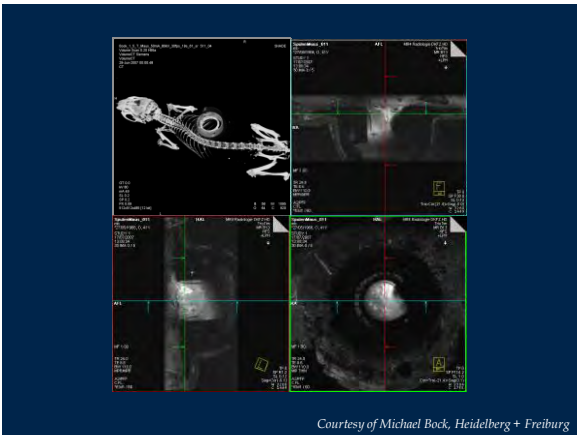
## Special small animal RF - Coils

- Skin Chamber Coil



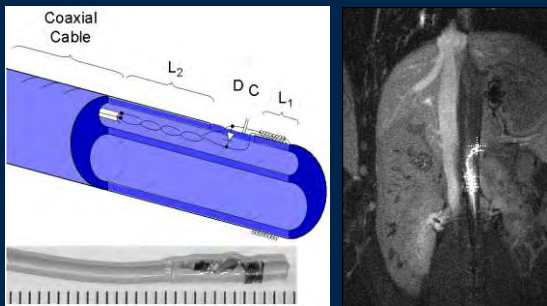
Bock M, et al. European Patent Application 1 681 017 A1





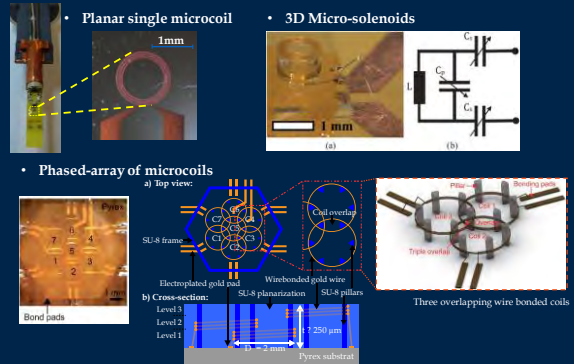
### Micro Coils

- Catheter tracking



Zühlsdorff S, et al., Magn Reson Med 52: 214-218 (2004)

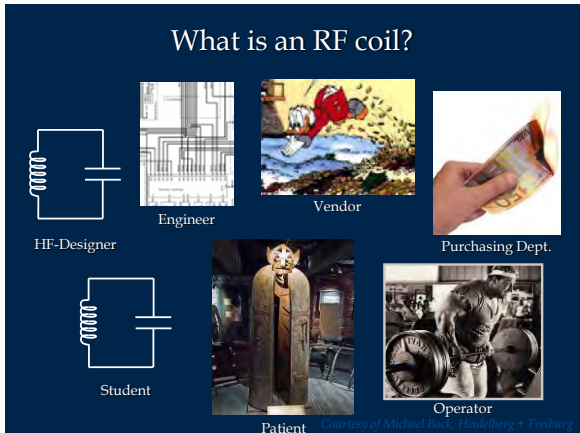
### Micro Coils



Courtesy of Oliver Gruschke + Vlad Badiita, Freiburg

### Purchasing RF coils

- Surface coils  
5000 € - 15.000 €, depending on size and nuclei
- Volume resonators  
15.000 € - 25.000 €, depending on design
- Phased array coils  
35.000 € - 70.000 €, depending on coil elements
- MRI CryoProbe  
255.000 € - 300.000 €, depending on field strength



Suggested literature on basics of MRI RF coils

- Link J, "The design of radiofrequency probes with homogeneous radiofrequency fields."  
NMR Basic Principles and Progress, Vol. 26 1992
- Hoult DL, "Signal to noise ratio of nuclear magnetic resonance experiment"  
Journal of Magnetic Resonance, Vol. 24, 1976
- Hoult DL, "NMR receiver – description and analysis of design"  
Journal of Magnetic Resonance, Vol. 12, 1978

WMIC 2012 Dublin,  
Wed. 5<sup>th</sup> of September, D. Elverfeldt:  
"Introduction on MRI Hardware, RF Coils"